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Emittance Measurements of Space Shuttle Orbiter Reinforced Carbon-Carbon

Jose M. Caram,
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Abstract

The spectral and total normal emittance of the Reinforced Carbon-Carbon (RCC) used on Space Shuttle Orbiter nose cap and wing leading edges has been measured at room temperature and at surface temperatures of 1200 to 2100°K. These measurements were made on virgin and two flown RCC samples. Room temperature directional emittance data were also obtained and were used to determine the total hemispherical emittance of RCC as a function of temperature. Results of the total normal emittance for the virgin samples showed good agreement with the current RCC emittance design curve; however, the data from the flown samples showed an increase in the emittance at high temperature possibly due to exposure from flight environments.

Introduction

The Space Shuttle Orbiter was the first operational hypersonic reentry vehicle flown with a nonablating reusable thermal protection system. The Leading Edge Sub-System (LESS) of the Orbiter, which includes the nose cap and wing leading edges, is protected from the extreme heat of reentry by the use of Reinforced Carbon-Carbon (RCC). RCC is a carbon composite possessing reasonable strength and low coefficient of thermal expansion which provides it with excellent resistance to thermal stress and shock.¹ The carbon-carbon is protected from oxidation by tetraethyl-ortho silicate (TEOS) impregnation and a silicon carbide (SiC) outer coating. The silicon carbide coating has a high total hemispherical emittance at normal operating temperatures around 1800°K which enhances the radiative heat rejection from the surface. However, under more severe conditions the emittance of the silicon carbide coating has been shown² to decrease as surface temperatures increase. Because of the effect the emittance of the silicon carbide coating has on the amount of heat transfer that the RCC surfaces are exposed to, accurate information on the variance of the total hemispherical emittance as a function of temperature of the SiC coating on the RCC is required.

Local heat transfer to the surface by convection under hypersonic flight conditions is determined from an energy balance, where heat addition is from the boundary layer heating and heat rejection is by radiation from the surface and conduction through the RCC. The accuracy of the determination of hot wall convective heat flux from flight or arc-plasma heated hypersonic wind tunnel data is directly dependent on the accuracy of the absolute value of the total hemispherical emittance of the coating at the temperature of the surface. The lower emittance would result in higher surface temperatures to maintain radiation equilibrium.

Since this thermal protection system is reusable, it is also of interest to evaluate changes in emittance with exposure to the hypersonic flight environment. Two RCC specimens were obtained from the right side wing panel 17 T-seal of the Space Shuttle Orbiter Atlantis. These specimens were cut from the T-seal at the location of the flow stagnation region. In this region, the heating to the wing panel during entry is at a maximum. In order to compare the data from the flown specimens and emittance data which was previously obtained,² virgin RCC samples were also tested. The present report summarizes the test procedures and test data including a determination of the total hemispherical emittance of the RCC/SiC coating as a function of temperature.

Test Samples

As was previously mentioned, two flown RCC samples (1 and 2) and two virgin RCC samples (4 and 5) were tested for emittance variation from room temperature to 2100°K. The flown samples were obtained from the

right side wing panel 17 T-seal on the Orbiter Atlantis (OV-104). The T-seal had been flown on nine Space Shuttle missions. The samples were cut in 4.5 cm x 2.5 cm sections, 0.64 cm thick, from the stagnation region of the panel. The stagnation region is the hottest portion of the T-seal during entry of the Orbiter. In order to perform the high temperature tests, these samples were further reduced to nominal dimensions of 1.2 cm x 1.2 cm. The virgin samples, obtained from LTV Corporation, were circular disks 1.9 cm in diameter and 0.64 cm in thickness. Two of the virgin samples were instrumented with a tungsten-5%-rhenium/tungsten-26%-rhenium thermocouple mounted along the centerline and placed just below the SiC coating. The thermocouples provided secondary surface temperature measurement support to the optical pyrometers.

Test Description

A Cary Model 17 Spectroflectometer was used to measure the room temperature near normal (6 degrees off normal) reflectance of the flown samples at wavelengths from 0.28 to 2.2 micrometers, whereas a Gier-Dunkle Model SP250 integrating sphere spectrophotometer was used for the virgin samples for wavelengths from 0.3 to 2.5 micrometers. At wavelengths between 2 and 25 micrometers, the reflectance was measured using the Gier-Dunkle Model HC-300 Heated Cavity Reflectometer. With this instrumentation, directional spectral reflectance data were obtained from near 0° to 75°. More details about this apparatus are provided in Ref. 3. Maximum uncertainty in spectral reflectance is typically ±0.01.

Data at temperatures ranging from 1200 to 2100°K were obtained using the Lockheed Missiles and Space Company (LMSC) Scanning Broadband Radiometer (SBR),⁴ with the front surface of the test sample heated with a continuous wave CO₂ laser in air at a pressure of 4.9kPa (37 Torr). The incident irradiance was uniform to within 5 percent over a 2 cm diameter spot at the center of the specimen. The SBR viewed a 0.8 cm diameter region centered in the area of uniform laser irradiation. A sketch of this test setup, along with the location from which the flown samples were taken, is shown in Figure 1. The filter wheel used has positions for eight filters which provided spectral data at wavelengths of 1.0, 2.08, 2.4, 2.73, 3.65, 4.76, 5.35, and 6.3 micrometers. Surface temperature of the sample was determined with optical pyrometers (0.65 and 4.5 micrometers). The SBR was calibrated using a high temperature blackbody over the range of 1100 to 2400°K to establish a correlation between the pyroelectric detector signal and radiant intensity. The estimated maximum uncertainty in the SBR data is ±0.04.

Test Results

Room Temperature Reflectance Data

Near-normal spectral reflectance data at room temperature were obtained for two of the virgin RCC samples (4 and 5). Since the room temperature transmittance of the SiC coating is low, the reflectance can be related to emittance (Emittance = 1 - Reflectance). Near-normal emittance as a function of wavelength (0.28 to 25 micrometers) is presented in Figure 2 and Table 1. The dip in the emittance at 10 to 13 micrometers is characteristic of the reststrahlen bands of the silicon carbide material.⁵ Spectral directional emittance data for these samples for wavelengths varying from 0.5 to 16 micrometers are shown in Figure 3. The data show good agreement between the two samples over the viewing angles and wavelengths tested. At the lower wavelengths, 0.5 to 2.0 micrometers, the emittance decreases slightly at the higher viewing angles indicating a small degree of specularity. However for the higher wavelengths, 4.0 to 16 micrometers, the emittance of the RCC/SiC coating begins to increase at the 60° viewing angle. It can also be seen that for the 10 to 16 micrometer range the emittance begins to spread, indicating the diffuse nature of the material at these higher wavelengths. Tables 2 and 3 also provide the directional emittance data.

Room temperature spectral normal reflectance values for both the inner and outer surfaces of the flown RCC samples, as well as data for the virgin samples over the same range, are shown in Figure 4 and in Table 4. The limited wavelength range of the data for the flown samples was due to the unsuitability of the samples to be machined to the size required by the HC300 instrument. The spectral normal emittance of the flown samples inner and outer surfaces is substantially higher than the virgin samples emittance at the 0.5 micrometer wavelength before converging at 1.5 micrometers. The fairly constant emittance, approximately 0.92, of the flown samples over the wavelength range tested may be an indication of the effect of repeated exposure to flight temperatures. The slight difference between the inner and outer surfaces in the visible and near IR wavelengths is well within the experimental error listed in this report.

Total normal emittance data at room temperature for the virgin and flown samples were determined by integrating the spectral data. Recall that the room temperature data for the flown specimen were limited from 0.4 micrometers to 2.2 micrometers and that there was good agreement at the higher wavelength with the virgin samples, Figure 4. Therefore, the total normal room temperature emittance of the flown samples outer and inner surfaces was found by assuming that the variation of the spectral emittance above the 2.2 micrometer wavelength was similar to the average of the virgin samples. Thus, the total normal emittance could be found for the flown samples for wavelengths between 0.4

and 24 micrometers. For virgin samples 4 and 5 the total normal room temperature emittance was 0.847 and 0.858 respectively, whereas for the flown specimen there was very little change between the outer and inner surfaces; they were 0.856 and 0.857, respectively.

Room temperature total hemispherical emittance for the virgin samples was obtained by integrating the directional emittance data (Fig. 3) for each of the wavelengths. This integration results in a ratio of hemispherical to normal emittance for each wavelength. These ratios were multiplied by the normal emittance for each wavelength and then integrated again over the wavelength band. Integration of the directional data for each wavelength was done from 0° to 90° and results in a ratio of hemispherical to normal emittance. If the data were obtained primarily between 20° and 75°, the emittance was assumed constant between 0° and 20°, and to have a cosine variation between the last angle and 90°. As a result, the ratios of hemispherical to normal emittance for each wavelength varied between 0.912 and 0.972, and hemispherical emittance totals at room temperature for virgin samples 4 and 5 were found to be 0.824 and 0.851, respectively. These data are summarized in Table 5.

High Temperature Emittance Data

Spectral normal emittance values for SiC coating from the two instrumented virgin samples and the two flown samples, both inner and outer surfaces, were also measured at surface temperatures of approximately 1200 to 2100°K with the SBR. Figures 5a and 5b and Tables 6 and 7 present the spectral normal emittance for virgin samples 4 and 5, respectively. The general trends of the high temperature spectral data are consistent with those reported by Wakefield⁶ for Arc-Jet results at a temperature of 2000°K. For both samples, a slight dip in the emittance can be seen in the 2 to 3 micrometer region with a strong decrease at 6 micrometers. At temperatures above 1900°K, a marked decrease in the emittance can be seen over the range of wavelengths. Indications of this decrease begin to appear at the 1 and 6 micrometer wavelengths when the temperature reaches approximately 1500°K. The spectral normal emittance data of the outer surface of the flown RCC samples (1 and 2) are seen in Figures 6a and 6b, respectively. The data show trends which are similar to those of the virgin samples. However, the dip between the 2 to 3 micrometer region is no longer discernible. Also, as surface temperatures increase, the decrease in the emittance for all wavelengths presented is less for the flown samples as compared to the virgin sample data. Both of these effects may be attributed to repeated exposure to flight reentry environments. These data are also provided in Table 8.

In Figures 7a and 7b and Table 9, the spectral normal emittance data for the inner surface of the flown specimens can be seen. There is little spectral dependence of the emittance of the inner surface and variation of spectral emittance with temperature is much less than that of the outer surface

measurements. Of particular interest in the figure is the lack of falloff above the 6 micrometer wavelength when compared to the virgin and flown specimen. In order to understand this insensitivity, emittance data for uncoated carbon-carbon⁷ are used for comparison. The agreement between the current data and the uncoated carbon-carbon indicates that there has been some modification of the SiC coating, which is typically between 0.051 cm and 0.1 cm in thickness, on the inner surface of the flown specimen. This modification may be due to either contact between the inner side of the T-seal and the RCC panel when they are exposed to the thermal and pressure stresses of flight, which may reduce the SiC coating thickness, or to the deposition of particulate from the various outgassing materials inside the wing leading edge cavity. Further analysis of the inner surface of the T-seal is required in order to determine this source.

High Temperature Total Normal and Total Hemispherical Emittance

Total normal emittance data were also obtained from the SBR tests. Figure 8a shows the total normal emittance of the inner surface of the flown RCC samples. Also included in the figure are the data for the uncoated carbon-carbon material which again shows that a modification of the SiC coating has occurred. The inner surface emittance data are essentially independent of temperature over the test temperature range, with an average value of 0.76. Unlike the inner surface data, the outer surface total normal emittance data for both flown specimens, seen in Figure 8b, decreases from a value of 0.86 at 1350°K to 0.75 at 2050°K. However, when compared to the virgin emittance data and the LTV design curve,² Figure 9, the total normal emittance for the outer surface of the flown RCC with the SiC coating shows excellent agreement except at the highest surface temperature test condition of 2050°K. At this temperature, the emittance for both flown specimens increases to 0.75 as compared to 0.63 for the virgin samples with an error of ± 0.04 . The increase in the emittance at this high temperature is beneficial in reducing the amount of heat energy absorbed into the material. The total normal data are also provided in Tables 10 and 11.

The total hemispherical emittance, which is the material property value needed for heat transfer computations, was computed from the test data by multiplying the total normal high temperature emittance values by the ratio of total hemispherical to total normal emittance for each of the samples obtained from the room temperature reflectance data. The use of these ratios for the high temperature hemispherical emittance values assumes that the directional distribution of emittance does not change with temperature. The total hemispherical emittance for the virgin and the flown RCC/SiC samples as a function of temperature are presented in Figure 10 and Table 12. Although slightly lower in magnitude than the total normal data, the flown outer surface data again show good agreement with the virgin samples except at the highest surface temperature test condition. The increase in the emittance at

the higher temperatures is believed to be caused by repeated exposure to flight environments and more flown samples should be obtained to verify this result.

Conclusions

Emittance tests have been conducted on both virgin and flown samples of RCC with a SiC coating. Room temperature spectral and directional reflectance measurements were obtained. Normal spectral and total emittance values have also been obtained for surface temperatures from 1200 to 2050° K. Total hemispherical emittance data at these temperatures were determined by assuming that the variation of the ratio of hemispherical to normal emittance data was constant with respect to temperature. The total normal emittance for the virgin material decreases from 0.89 to 0.63 over this temperature range. Using the room temperature directional data, the total hemispherical emittance data varied from 0.87 to 0.613. Comparable emittance values were measured for the flown RCC samples at the lower temperatures, but the emittance only decreased to 0.75 for the total normal and to 0.72 for the total hemispherical at the higher temperatures. This trend suggests that the entry flight environment has affected the emittance characteristics of the RCC/SiC coating. However, only a limited amount of data was obtained at the high temperatures and further tests would be required to confirm this trend.

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Table 1 - Virgin RCC Room Temperature Normal Emittance

Wavelength (μm)	Sample 4	Sample 5	Wavelength (μm)	Sample 4	Sample 5
0.300	0.810	0.820	11.5	0.762	0.770
0.500	0.792	0.813	12.0	0.719	0.732
0.800	0.832	0.834	12.5	0.693	0.709
0.900	0.842	0.843	13.0	0.770	0.788
1.00	0.868	0.873	13.5	0.794	0.812
1.20	0.889	0.890	14.0	0.803	0.820
1.50	0.900	0.910	14.5	0.808	0.825
1.75	0.910	0.911	15.0	0.812	0.830
2.00	0.918	0.919	15.5	0.815	0.830
2.50	0.929	0.928	16.0	0.818	0.835
3.00	0.937	0.936	16.5	0.816	0.830
3.50	0.938	0.938	17.0	0.812	0.832
4.00	0.937	0.937	17.5	0.818	0.832
4.50	0.935	0.935	18.0	0.812	0.832
5.00	0.930	0.933	18.5	0.811	0.828
5.50	0.926	0.928	19.0	0.820	0.838
6.00	0.924	0.928	19.5	0.810	0.827
6.50	0.912	0.914	20.0	0.818	0.836
7.00	0.912	0.914	20.5	0.812	0.830
7.50	0.910	0.913	21.0	0.810	0.832
8.00	0.911	0.916	21.5	0.803	0.825
8.50	0.908	0.915	22.0	0.805	0.825
9.00	0.895	0.912	22.5	0.801	0.820
9.50	0.892	0.910	23.0	0.808	0.827
10.0	0.909	0.913	23.5	0.811	0.828
10.5	0.862	0.863	24.0	0.827	0.833
11.0	0.808	0.812			

Table 2 - Virgin RCC Sample 4 Room Temperature Directional Emittance

View Angle	0.5 μm	1.0 μm	1.5 μm	2.0 μm	4.0 μm	7.0 μm	10 μm	13 μm	16 μm
0°	0.790	0.868	0.900	0.917					
20°	0.798	0.870	0.900	0.915	0.938	0.913	0.911	0.775	0.822
30°	0.790	0.867	0.900	0.915	0.935	0.910	0.910	0.772	0.820
40°	0.775	0.860	0.896	0.912	0.937	0.910	0.906	0.770	0.805
50°	0.763	0.851	0.888	0.905	0.932	0.904	0.900	0.762	0.801
60°	0.755	0.848	0.880	0.899	0.928	0.902	0.893	0.760	0.812
65°					0.928	0.906	0.896	0.775	
70°	0.742	0.832	0.870	0.888					
75°	0.738	0.828	0.855	0.870					

Table 3 - Virgin RCC Sample 5 Room Temperature Directional Emittance

View Angle	0.5 μm	1.0 μm	1.5 μm	2.0 μm	4.0 μm	7.0 μm	10 μm	13 μm	16 μm
0°	0.813	0.875	0.903	0.918					
20°	0.811	0.875	0.903	0.916	0.938	0.915	0.920	0.796	0.838
30°	0.810	0.870	0.901	0.916	0.938	0.915	0.918	0.795	0.835
40°	0.805	0.865	0.900	0.914	0.937	0.915	0.918	0.794	0.830
50°	0.800	0.863	0.897	0.912	0.932	0.910	0.912	0.787	0.825
60°	0.790	0.858	0.892	0.910	0.928	0.910	0.911	0.780	0.821
65°					0.935	0.915	0.912	0.790	0.828
70°	0.781	0.848	0.880	0.900	0.940	0.915	0.915	0.796	0.838
75°	0.770	0.840		0.891					

Table 4 - Virgin and Flown RCC Samples Room Temperature Normal Emittance

Wavelength (μm)	Sample 4	Sample 5	Flown Outer Surface	Flown Inner Surface
0.400	0.810	0.820	0.911	0.931
0.500	0.792	0.814	0.912	0.925
0.700	0.832	0.835	0.912	0.923
0.800	0.842	0.844	0.911	0.922
1.00	0.868	0.875	0.915	0.930
1.20	0.888	0.890	0.918	0.930
1.50	0.900	0.910	0.920	0.930
1.70	0.910	0.912	0.921	0.932
2.00	0.918	0.918	0.925	0.934
2.20	0.922	0.922	0.922	0.934

Table 5 - Virgin RCC Spectral Hemispherical Emittance

Wavelength (μm)	Sample 4			Sample 5		
	Normal Emittance	Hemis./ Normal	Hemis. Emittance	Normal Emittance	Hemis./ Normal	Hemis. Emittance
0.500	0.792	0.954	0.756	0.813	0.969	0.788
1.00	0.868	0.965	0.838	0.873	0.969	0.846
1.50	0.900	0.968	0.871	0.910	0.949	0.864
2.00	0.918	0.966	0.887	0.919	0.972	0.893
4.00	0.937	0.939	0.880	0.937	0.962	0.901
7.00	0.912	0.939	0.856	0.914	0.963	0.880
10.0	0.909	0.937	0.852	0.913	0.966	0.882
13.0	0.770	0.942	0.725	0.788	0.968	0.763
16.0	0.818	0.912	0.746	0.835	0.959	0.801

Table 6 - Virgin RCC Sample 4 Spectral Normal Emittance

Wavelength (μm)	1354°K	1504°K	1770°K	1915°K	2037°K
1.00	0.850	0.830	0.700	0.600	0.550
2.08	0.890	0.870	0.840	0.740	0.620
2.40	0.850	0.810	0.790	0.730	0.670
2.73			0.930	0.840	0.710
3.65	0.910	0.900	0.870	0.810	0.740
4.76	0.870	0.820	0.790	0.750	0.720
5.35	0.850	0.790	0.770	0.690	0.630
6.30	0.625		0.410	0.430	0.440

Table 7 - Virgin RCC Sample 5 Spectral Normal Emittance

Wavelength (μm)	1367°K	1506°K	1690°K	1772°K
1.00	0.840	0.810	0.740	0.680
2.08			0.820	0.810
2.40	0.850	0.830	0.840	0.800
2.73	0.930		0.880	0.910
3.65	0.900		0.910	0.890
4.76	0.870	0.810	0.830	0.800
5.35			0.800	0.750
6.30	0.700	0.470	0.480	0.400

Table 8A - Flown RCC Outer 1 Spectral Normal Emittance

Wavelength (μm)	1384°K	1583°K	1724°K	2050°K
1.00	0.810	0.770	0.750	0.690
2.08	0.830		0.790	0.720
2.40	0.860	0.880	0.780	0.740
2.73	0.855	0.790	0.800	0.760
3.65	0.860	0.890	0.840	0.760
4.76	0.825	0.780	0.760	0.730
5.35	0.805	0.780	0.760	0.730
6.30	0.500	0.540	0.530	0.440

Table 8B - Flown RCC Outer 2 Spectral Normal Emittance

Wavelength (μm)	1368°K	1562°K	1701°K	2053°K
1.00	0.780	0.750	0.740	0.700
2.08	0.790	0.780	0.760	0.740
2.40	0.850	0.890	0.790	
2.73	0.880	0.850	0.740	0.770
3.65			0.830	0.740
4.76	0.750		0.760	0.780
5.35			0.750	
6.30	0.450		0.530	0.500

Table 9A - Flown RCC Inner 1 Spectral Normal Emittance

Wavelength (μm)	1357°K	1550°K	1770°K	1989°K
1.00	0.730	0.760	0.740	
2.08		0.770	0.730	
2.40		0.730		0.710
2.73			0.720	0.700
3.65	0.770	0.740	0.750	0.730
4.76	0.770	0.750	0.760	0.700
5.35		0.710	0.715	0.695
6.30	0.620	0.650		0.645

Table 9B - Flown RCC Inner 2 Spectral Normal Emittance

Wavelength (μm)	1423°K	1611°K	1759°K	2153°K
1.00	0.720	0.780	0.740	0.700
2.08		0.795	0.700	0.760
2.40	0.740		0.750	
2.73			0.730	
3.65	0.780		0.750	0.730
4.76	0.780		0.770	0.700
5.35	0.730	0.720	0.740	0.700
6.30	0.650	0.670	0.640	0.600

Table 10 - Flown RCC Total Normal Emittance

Temp. (°K)	Inner Surface 1	Temp. (°K)	Inner Surface 2	Temp. (°K)	Outer Surface 1	Temp. (°K)	Outer Surface 2
1358.0	0.770	1420.0	0.770	1380.0	0.875	1370.0	0.840
1550.0	0.760	1610.0	0.765	1580.0	0.785	1565.0	0.790
1770.0	0.735	1760.0	0.755	1722.0	0.825	1700.0	0.800
1990.0	0.730	2150.0	0.735	2050.0	0.740	2057.0	0.760

Table 11 - Composite Total Normal Emittance for RCC

Temp. (°K)	LTV Design	Temp. (°K)	Virgin	Temp. (°K)	Flown Outer
533.00	0.825	300.0	0.853 (avg.)	300.0	0.856
756.00	0.863	1205.0	0.890	1370.0	0.840
1033.0	0.890	1350.0	0.870	1380.0	0.875
1200.0	0.900	1360.0	0.840	1565.0	0.790
1311.0	0.900	1505.0	0.830	1580.0	0.785
1422.0	0.880	1505.0	0.810	1700.0	0.800
1589.0	0.833	1670.0	0.800	1722.0	0.825
1756.0	0.770	1695.0	0.770	2050.0	0.740
1922.0	0.694	1760.0	0.750	2057.0	0.760
2089.0	0.610	1770.0	0.790		
		1910.0	0.670		
		1915.0	0.700		
		2040.0	0.630		

Table 12 - Composite Total Hemispherical Emittance for RCC

Temp. (°K)	Virgin	Temp. (°K)	Flown Outer
1205.0	0.86600	1370.0	0.82200
1350.0	0.84700	1380.0	0.85600
1360.0	0.83300	1565.0	0.77300
1505.0	0.80400	1580.0	0.76800
1505.0	0.80800	1700.0	0.78200
1670.0	0.77800	1722.0	0.80700
1695.0	0.76400	2050.0	0.72400
1760.0	0.74400	2057.0	0.74300
1770.0	0.76900		
1910.0	0.66500		
1915.0	0.68100		
2040.0	0.61300		

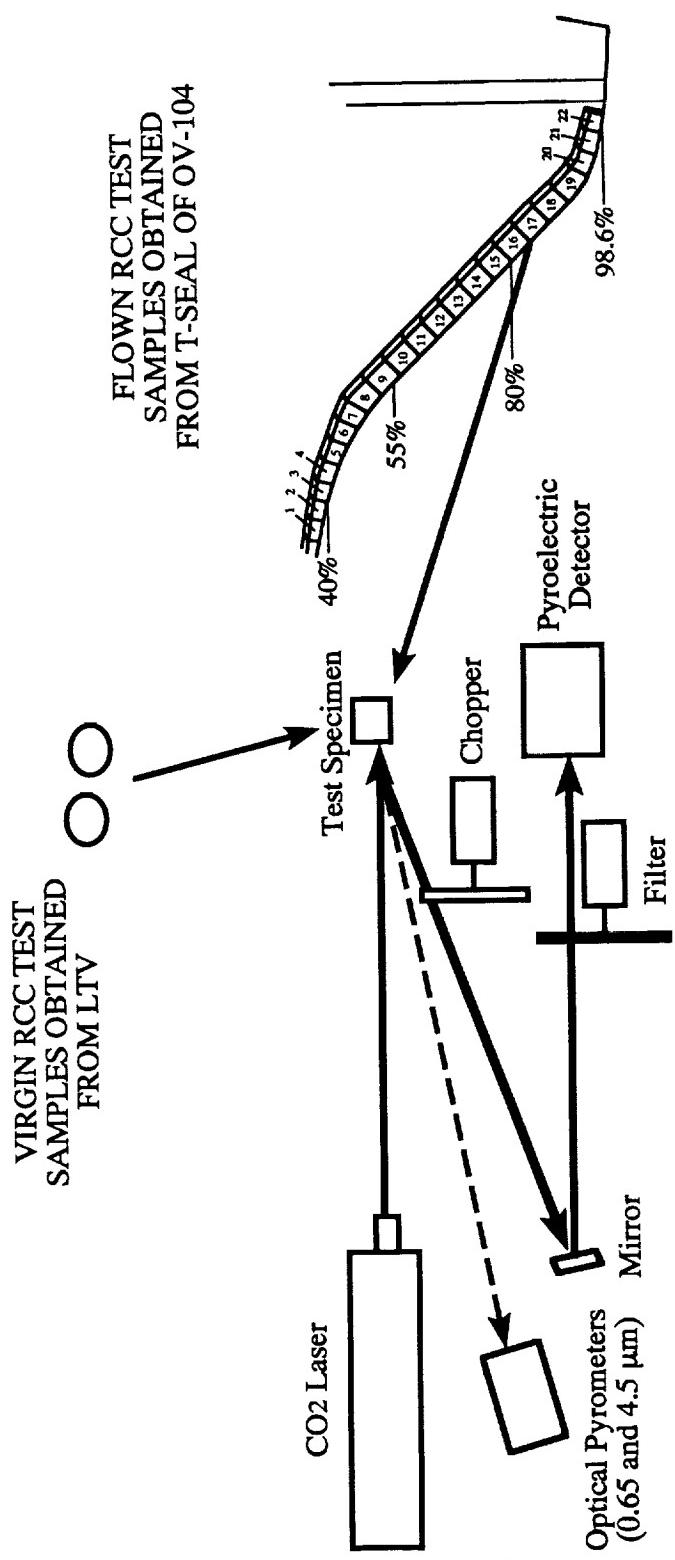


Figure 1 - Sketch of Scanning Broadband Radiometer Test Setup at
 Lockheed Palo Alto Research Laboratory

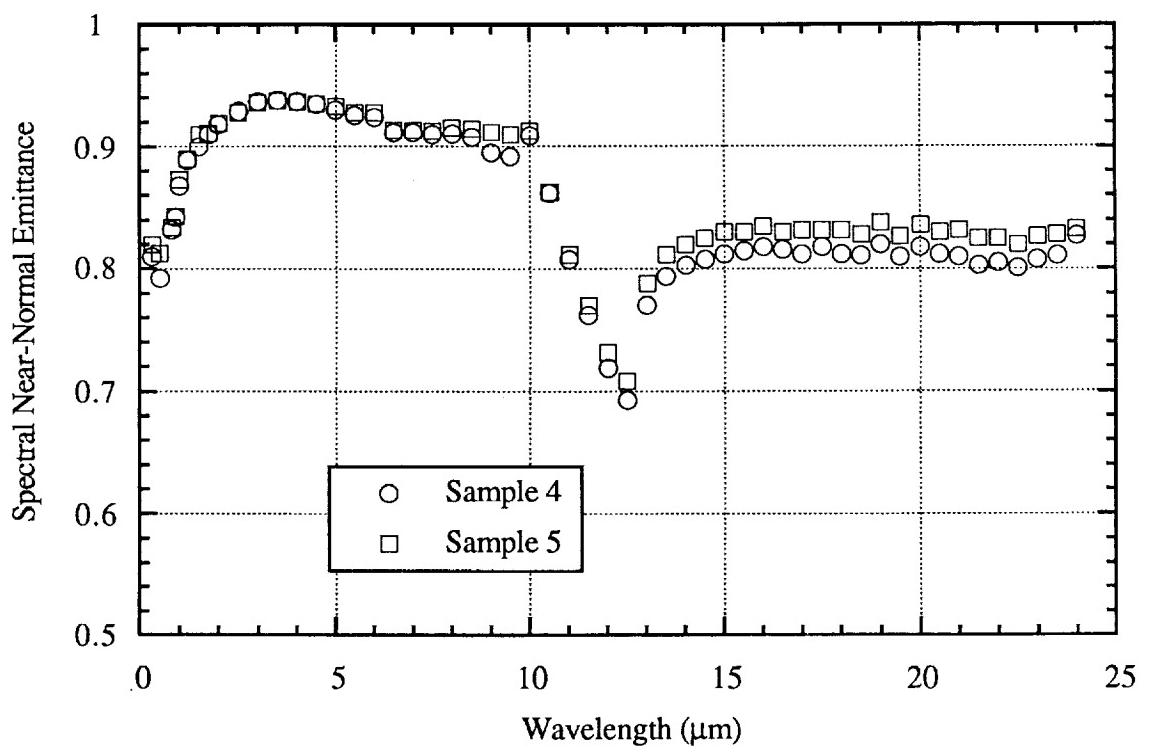


Figure 2 - Spectral Near-Normal Emittance at Room Temperature for Virgin RCC

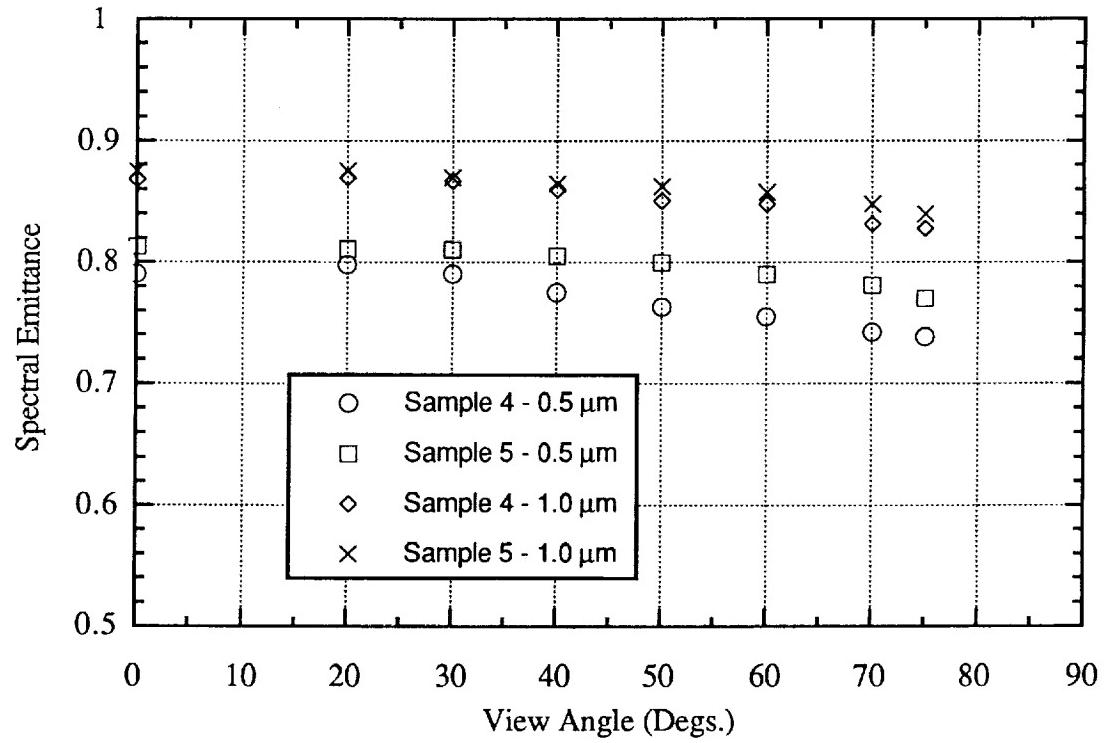
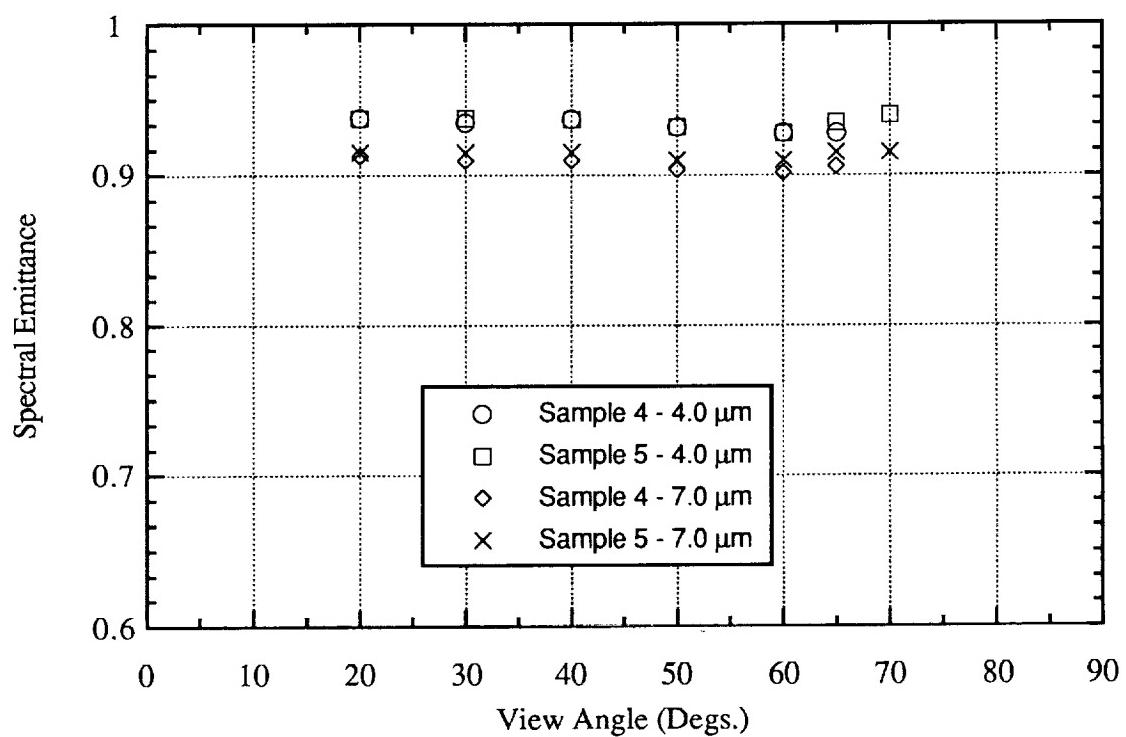
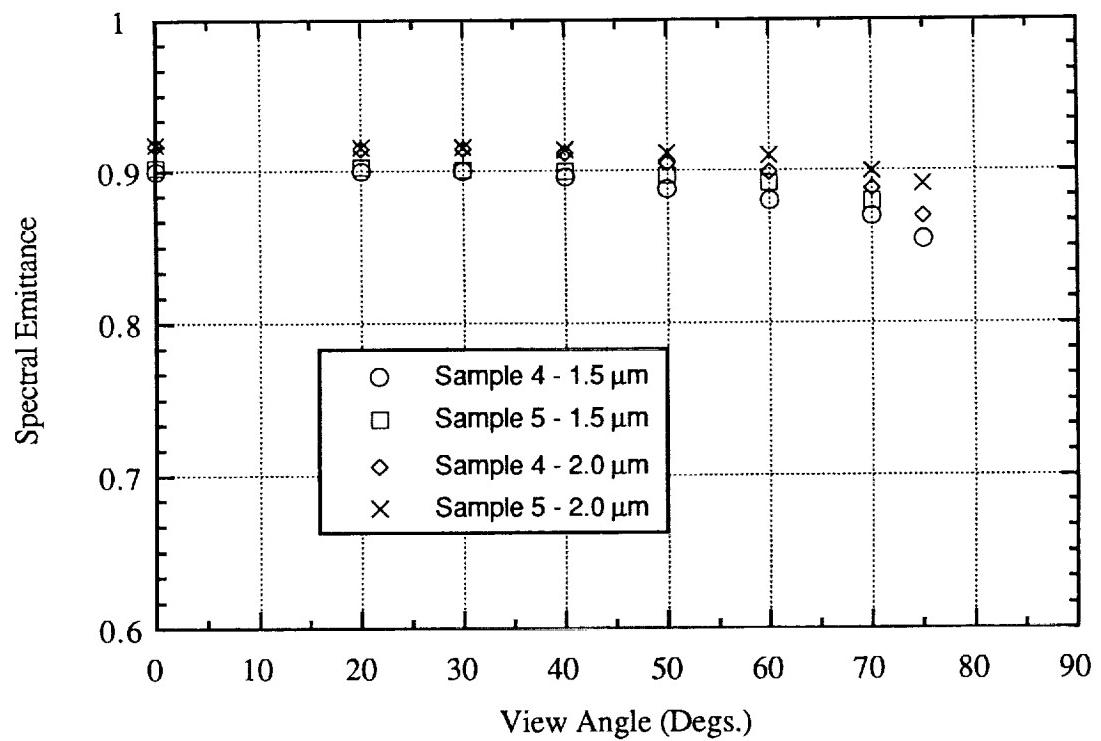


Figure 3A - Room Temperature Directional Emittance Data for Virgin RCC Samples



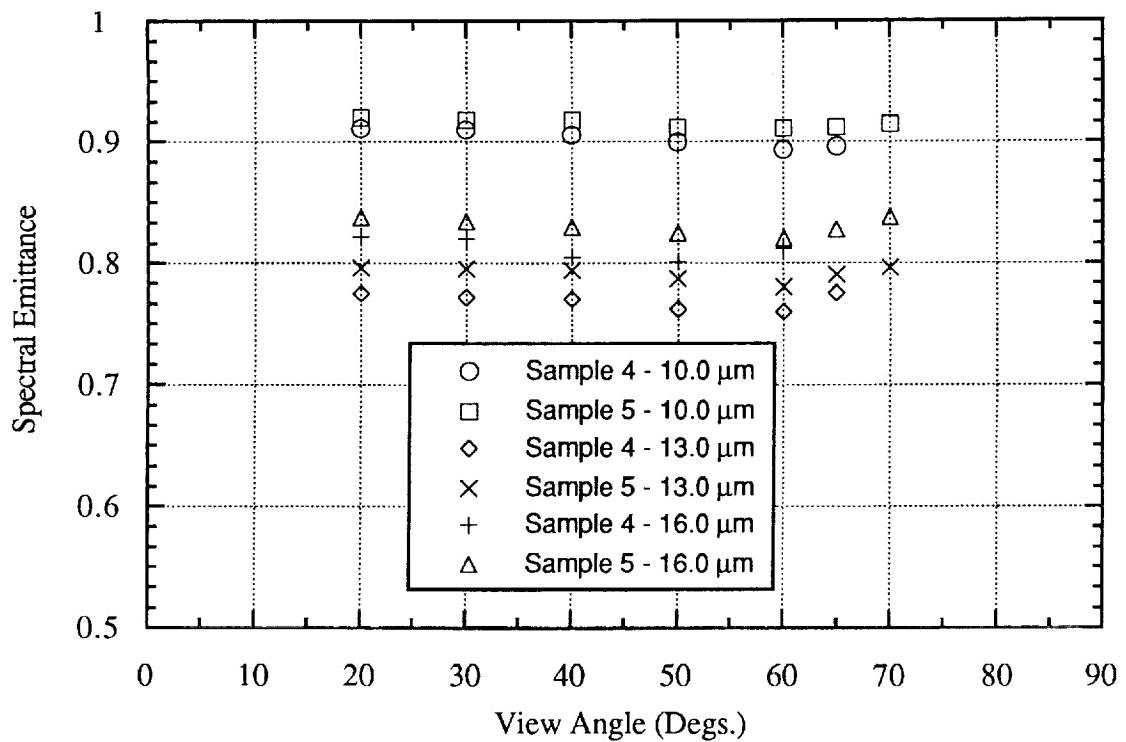


Figure 3D - Room Temperature Directional Emittance Data for Virgin RCC Samples

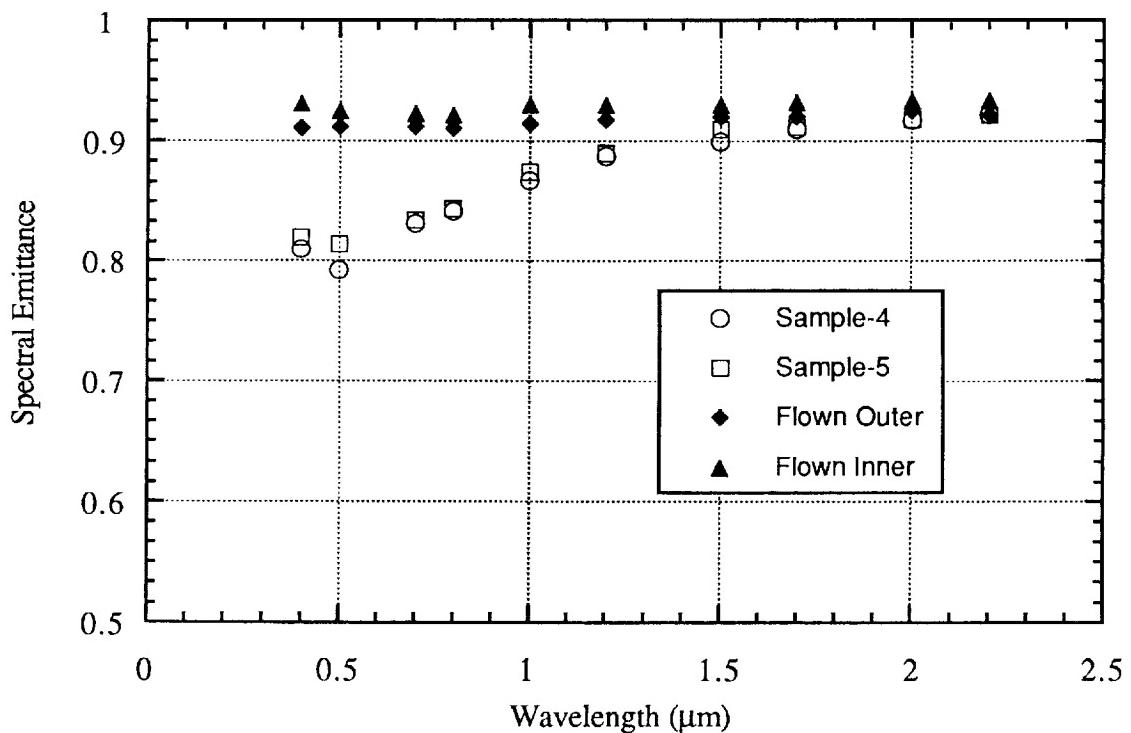


Figure 4 - Virgin and Flown RCC Spectral Normal Emittance at Room Temperature

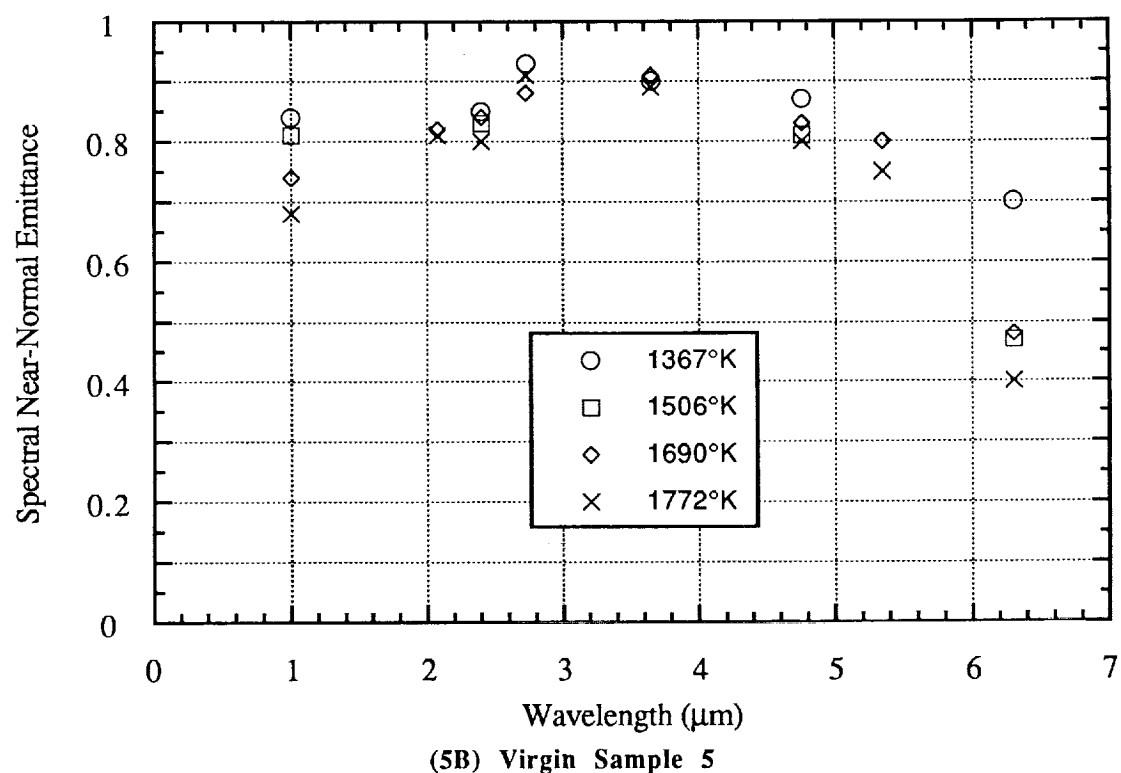
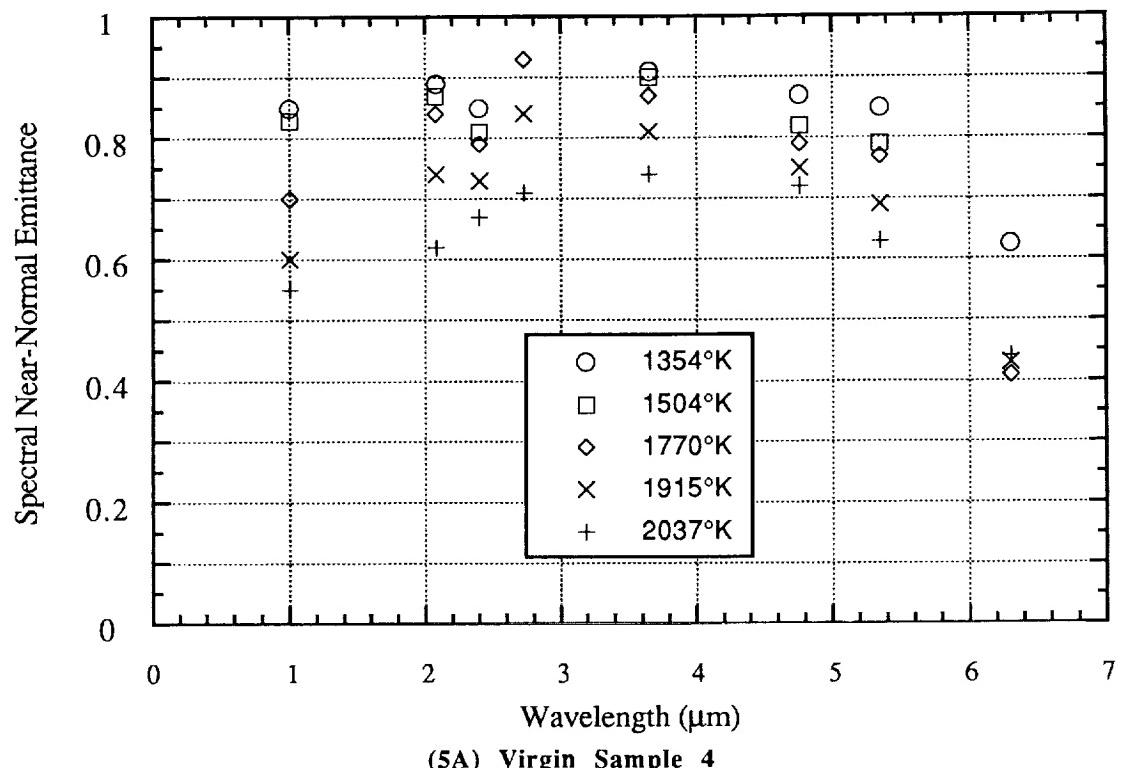
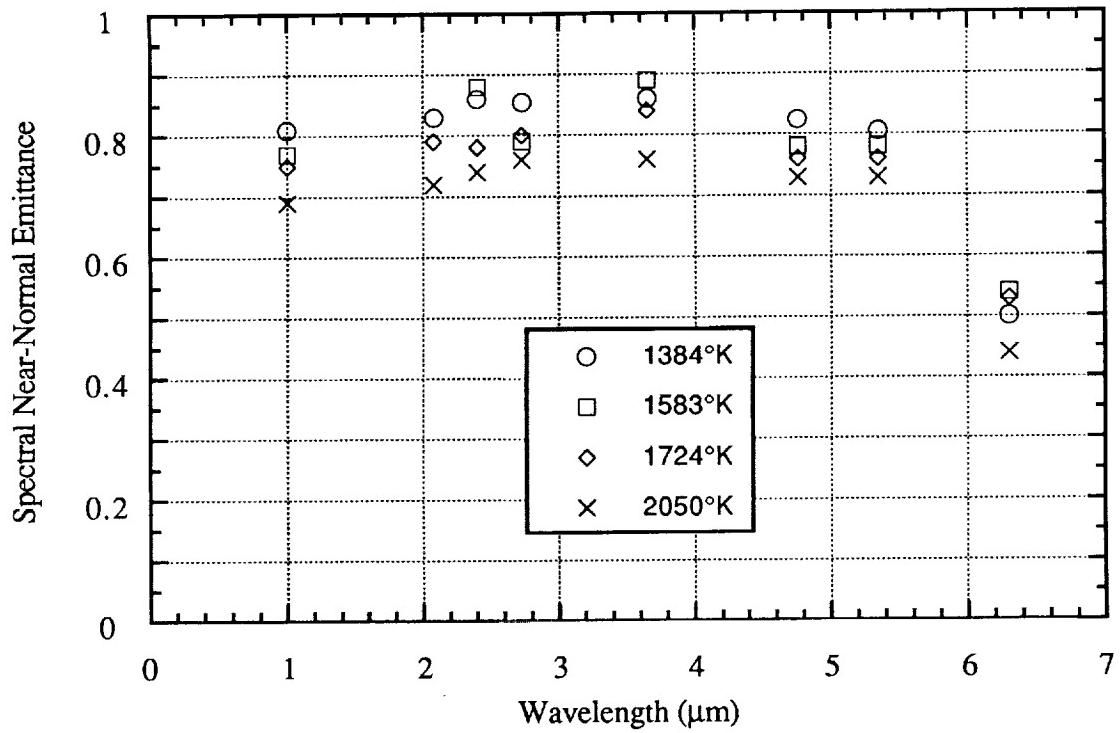
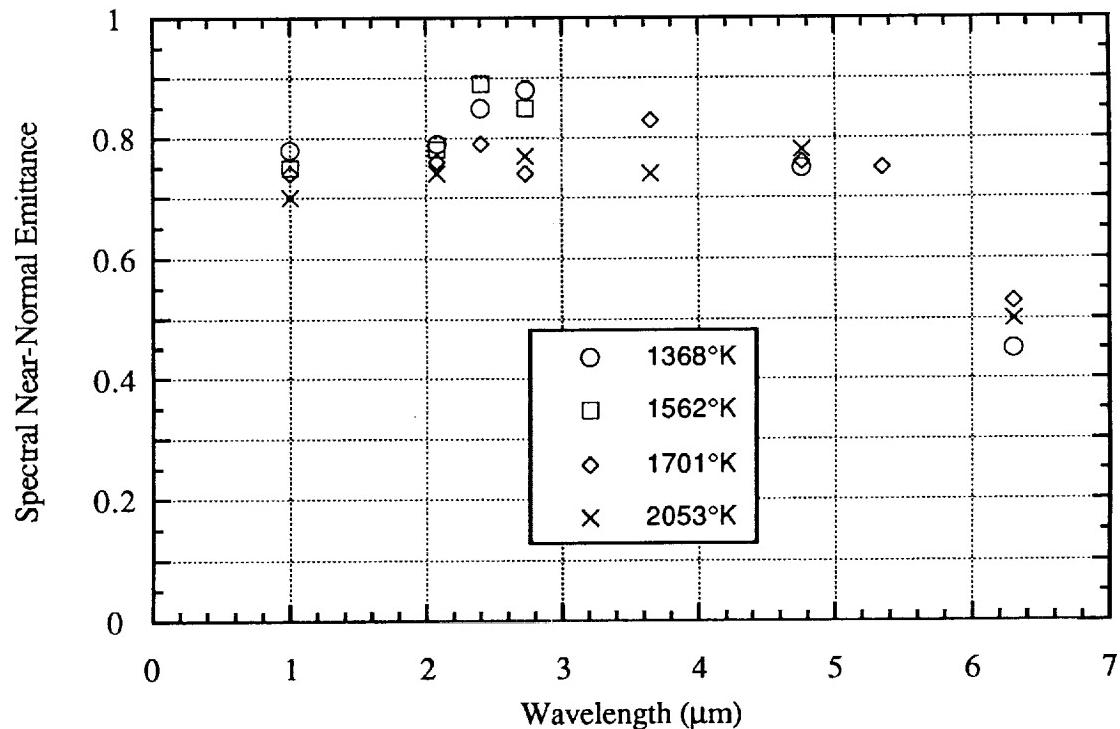


Figure 5 - High Temperature Near-Normal Spectral Emittance Data for Virgin RCC



(6A) Flown RCC - Outer Surface - Sample 1



(6B) Flown RCC - Outer Surface - Sample 2

Figure 6 - High Temperature Near-Normal Spectral Emittance Data for Flown RCC

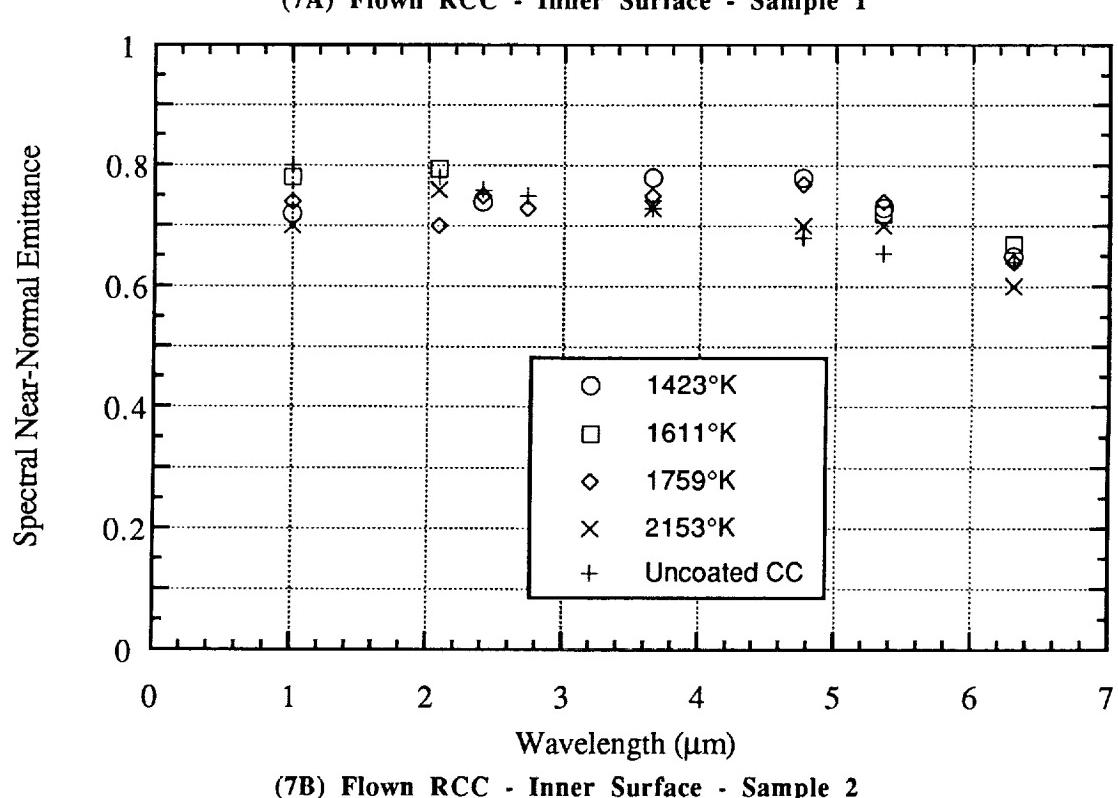
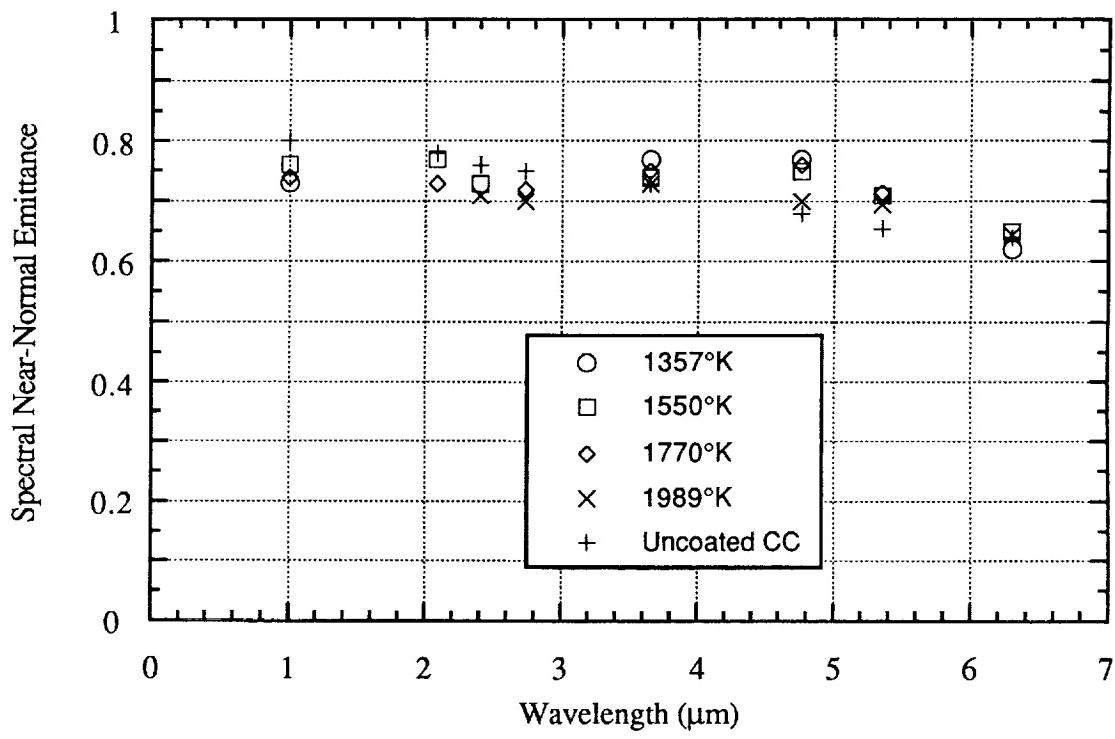


Figure 7 - High Temperature Near-Normal Spectral Emittance Data for Flown RCC

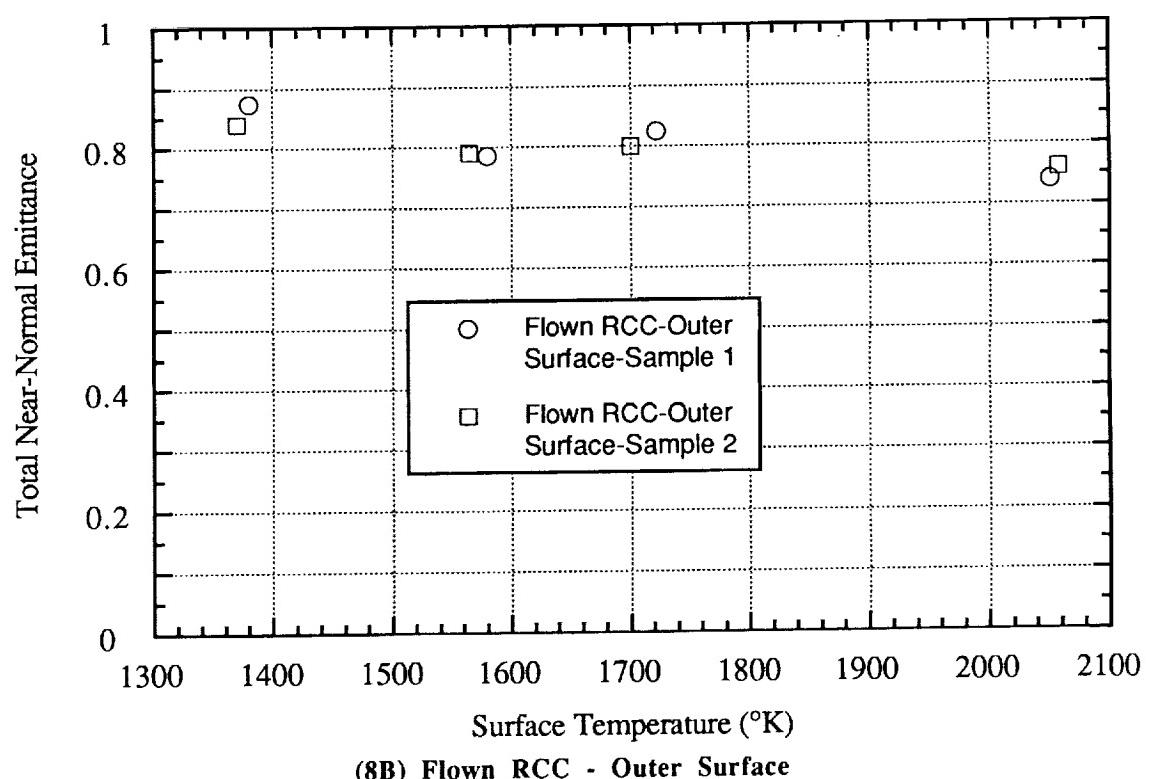
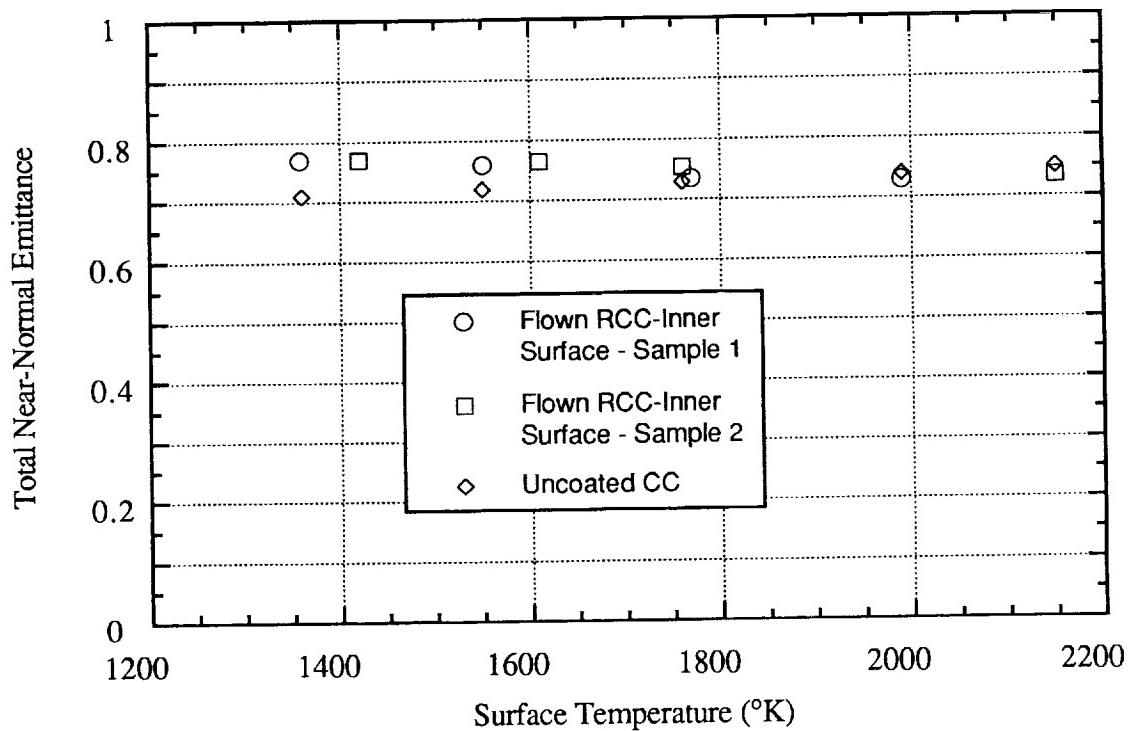


Figure 8 - High Temperature Total Normal Emittance Data for Flown RCC Samples

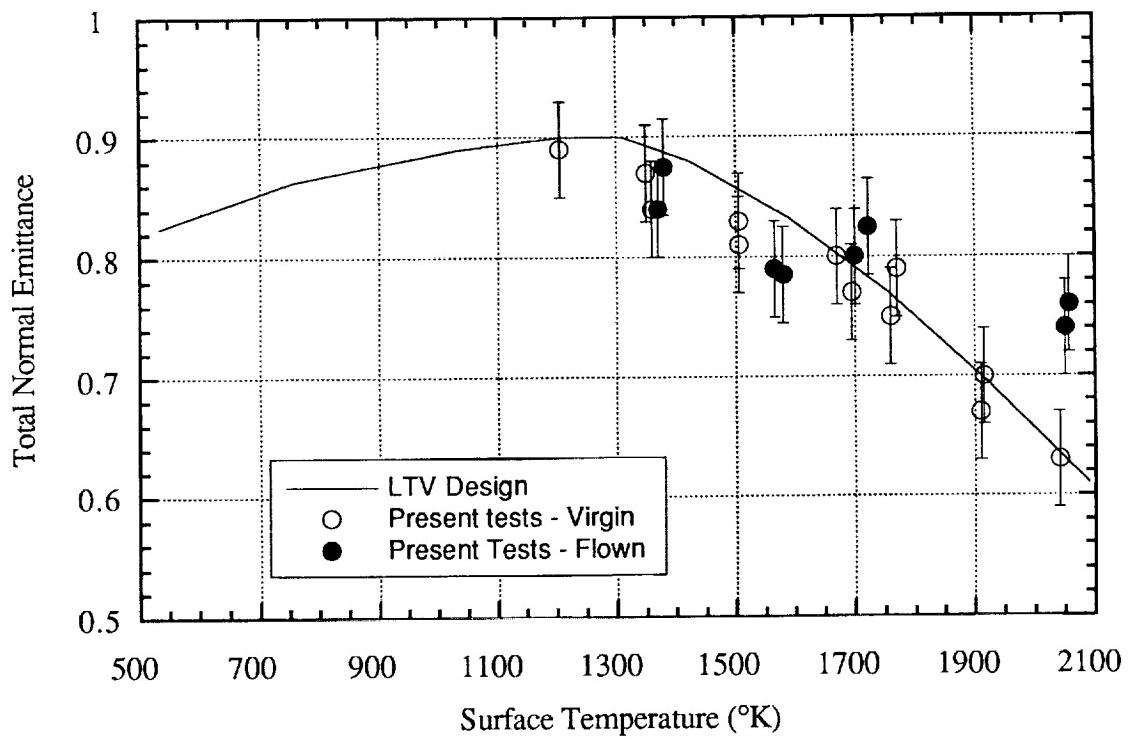


Figure 9 - Comparison of High Temperature Total Normal Emittance

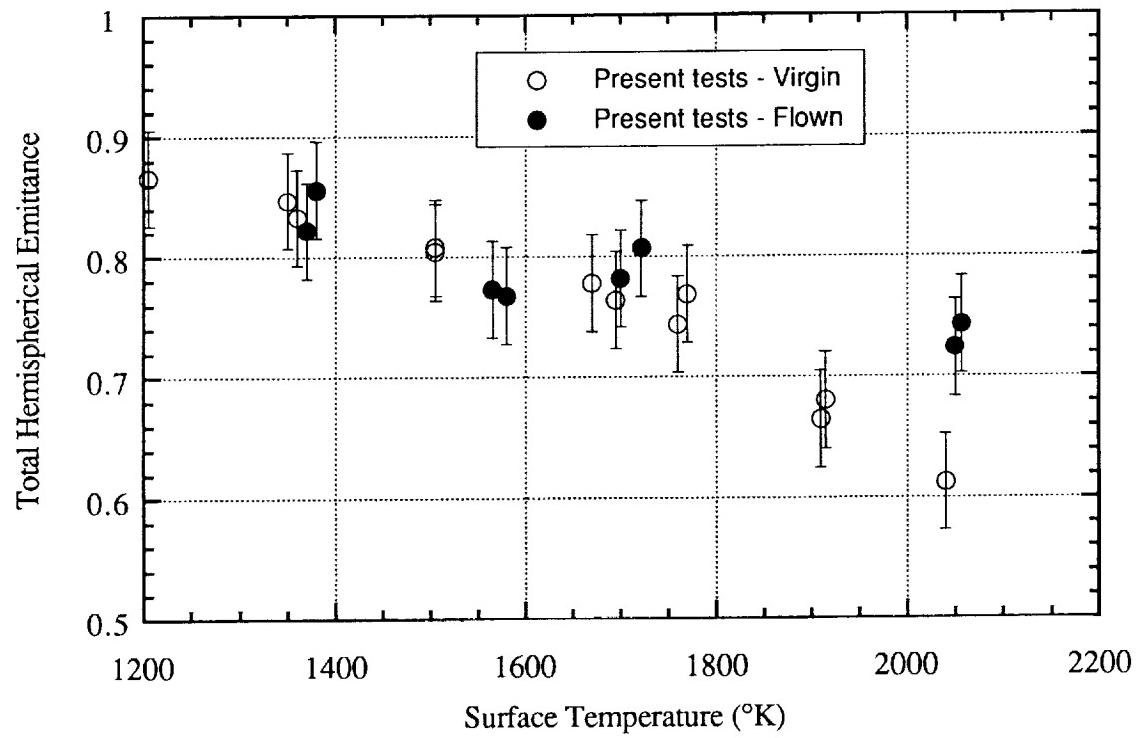


Figure 10 - Comparison of High Temperature Total Hemispherical Emittance

REPORT DOCUMENTATION PAGE

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